



Lecture 8 – Turbocharger Modeling

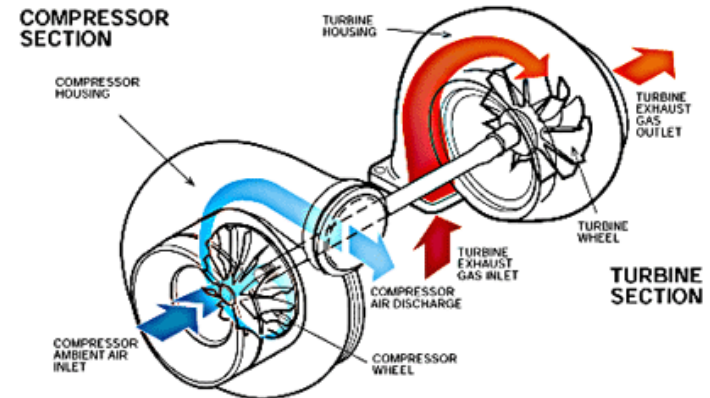
System Modeling – Institute for Dynamic Systems and Control (IDSC)

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Dr. Guillaume Ducard

Lecture Overview

■ Turbocharger modeling

- Turbine & Compressor
- Causality diagram
- Inputs, outputs
- Maps and operation



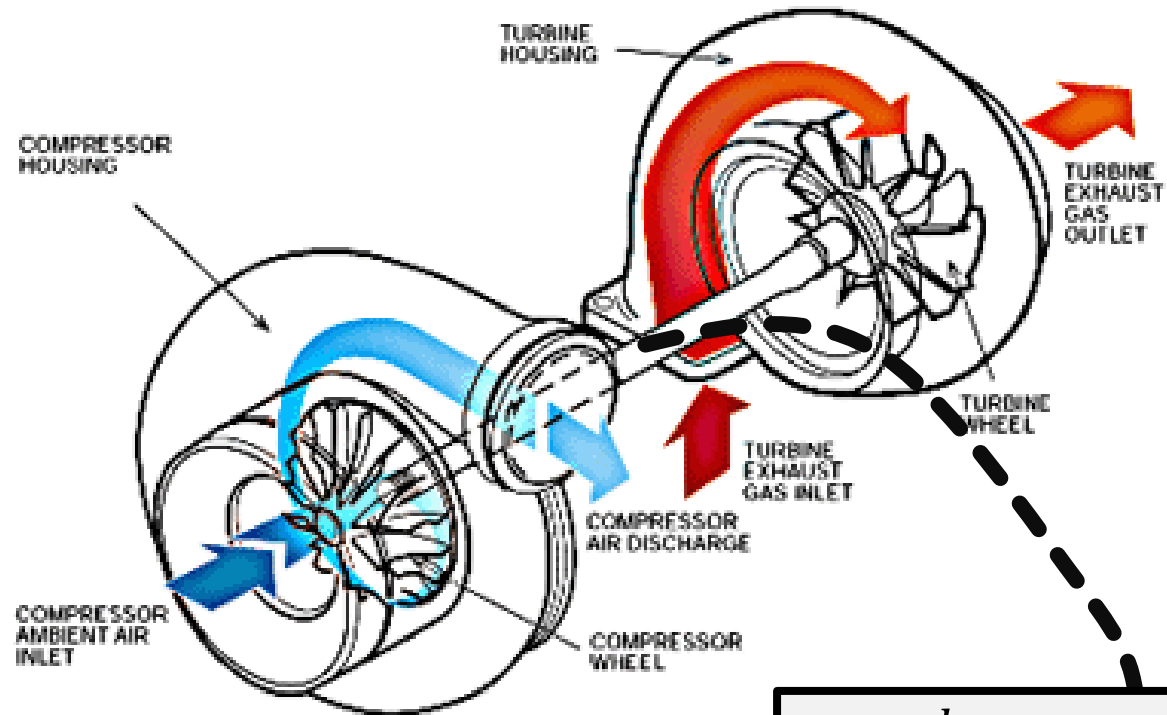
Source: <https://auto.howstuffworks.com/turbo2.htm>

■ Turbocharged internal combustion engines

- Engine power modeling
- Naturally aspirated (NA) Vs turbocharged (TC) engines
- Benefits of turbocharging
- F1 electrified turbocharger

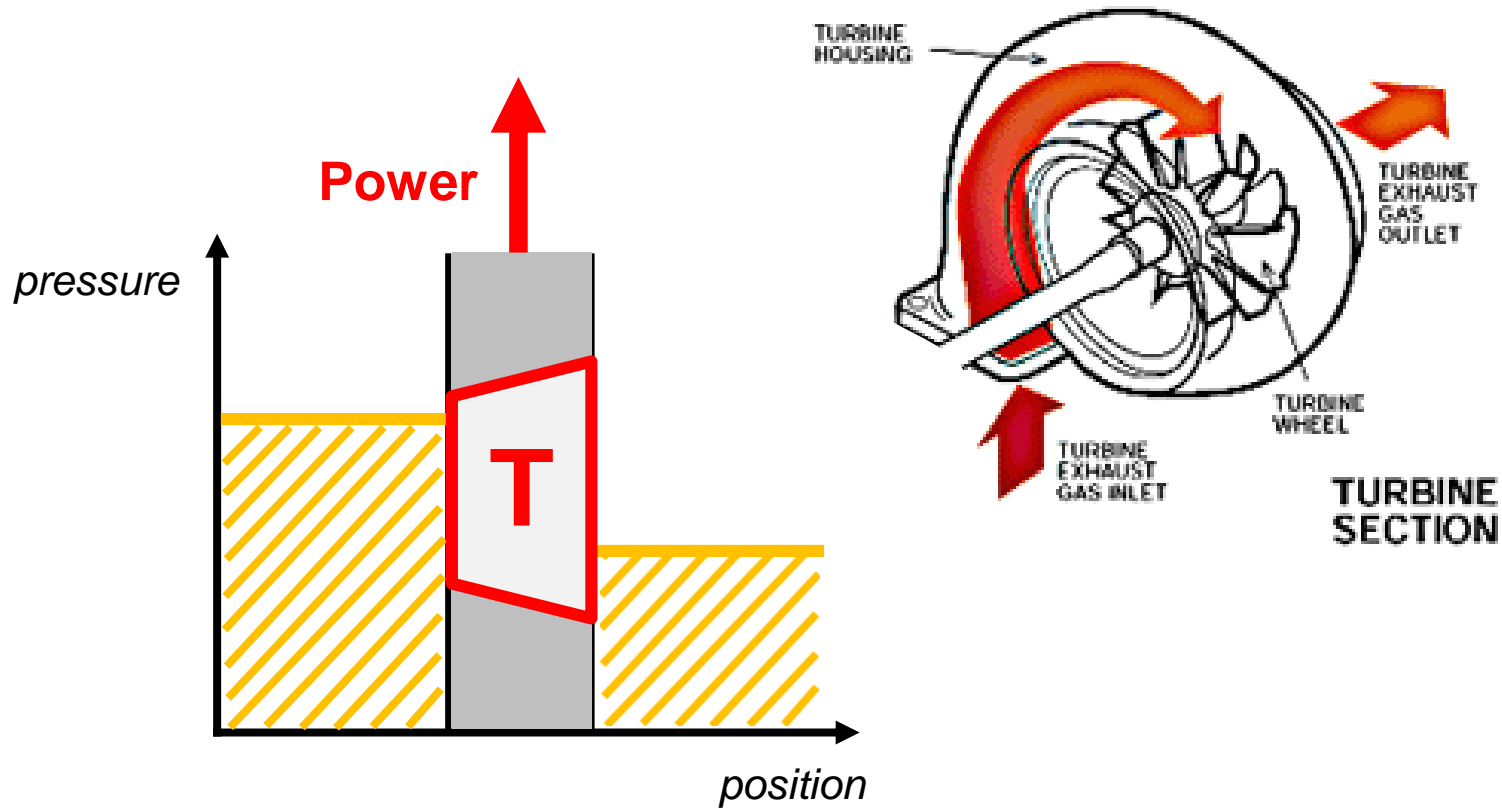


Turbocharger

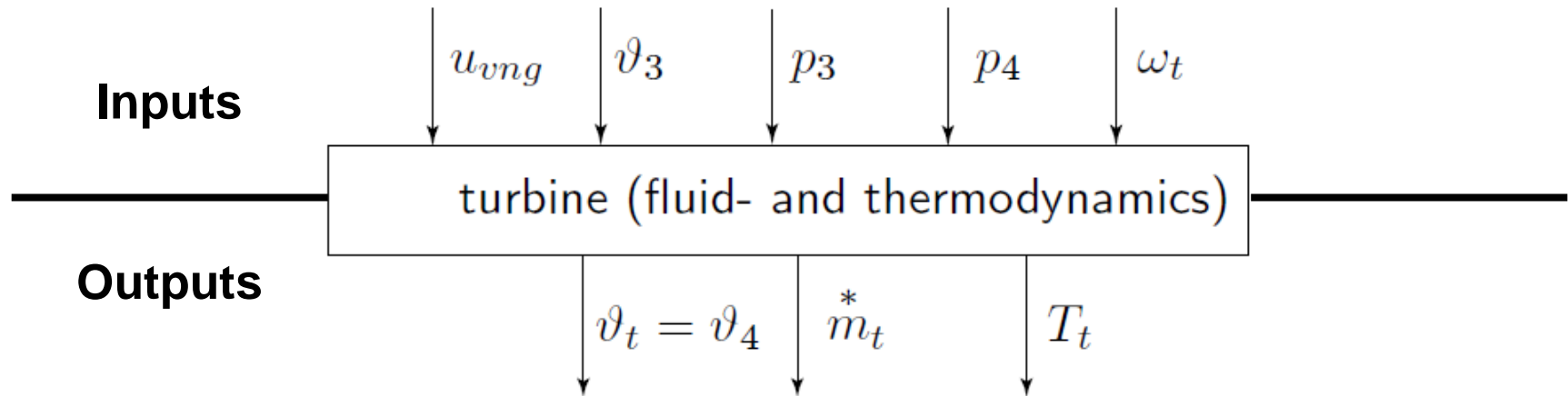


$$\Theta_{tc} \cdot \frac{d\omega_{tc}}{dt} = T_t - T_c + T_{ext}$$

Turbine



Turbine – Causality Diagram



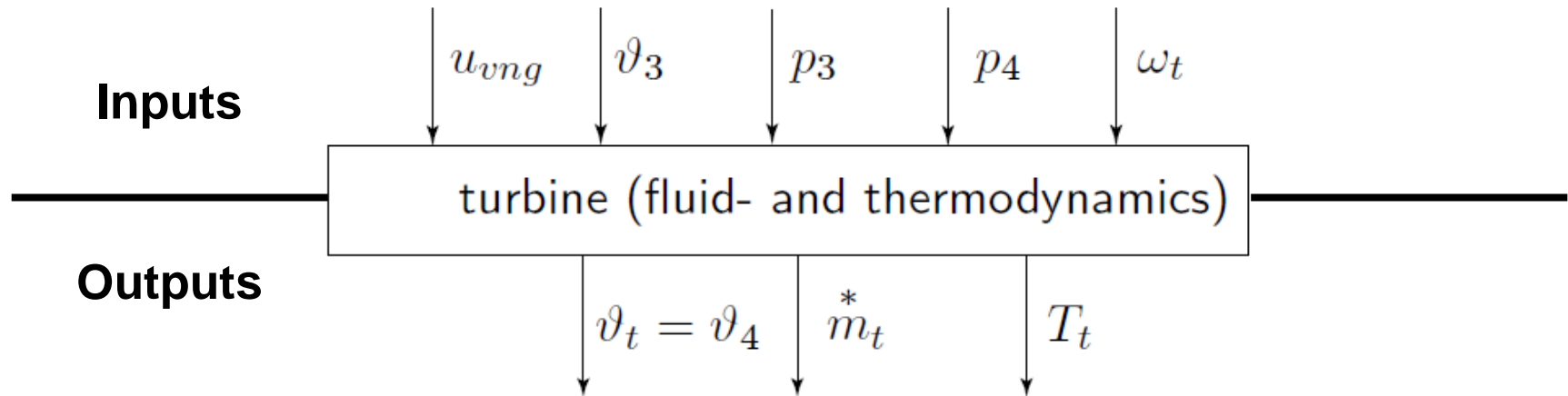
Inputs

- ϑ_3 : Temperature before the turbine [K]
- p_3 : pressure before the turbine [Pa]
- p_4 : pressure after the turbine [Pa]
- ω_t : Turbine speed [rad/s]
- u_{vng} : Variable nozzle geometry control input [–]

}

$$\Pi_t = \frac{p_3}{p_4} = \frac{p_{bef,t}}{p_{aft,t}}$$

Turbine – Causality Diagram



Outputs

- ϑ_4 : Temperature of the flow exiting the turbine [K]
- \dot{m}_t : Mass flow through the turbine [Kg/s]
- T_t : Torque generated by the turbine [Nm]

Turbine – Outputs

- **Temperature** of the flow exiting the turbine

$$\vartheta_4 = \vartheta_3 \cdot \left[1 - \eta_t \cdot \left(1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right) \right]$$

- **Mass Flow** through the turbine

$$\dot{m}_t = \frac{p_3}{p_{ref,0}} \cdot \sqrt{\frac{\vartheta_{ref,0}}{\vartheta_3}} \cdot \dot{\mu}_t$$

$$\Pi_t = \frac{p_3}{p_4} = \frac{p_{bef,t}}{p_{aft,t}}$$

- **Torque** produced by the turbine

$$T_t = \frac{P_t}{\omega_t} = \frac{\dot{m}_t \cdot c_p \cdot \vartheta_3}{\omega_t} \cdot \left[1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right] \cdot \eta_t$$

Turbine – Outputs derivation

Open system

$$\frac{dE}{dt} = \dot{H}_{in} - \dot{H}_{out} - \dot{W}_t + \dot{Q}$$

- Turbine does **not store energy** over time $\Rightarrow \frac{dE}{dt} = 0$
- Turbine is assumed to be **adiabatic** (no heat transfer) $\Rightarrow \dot{Q} = 0$

$$P_t = \dot{W}_t = \dot{H}_{in} - \dot{H}_{out} = \dot{m}_t \cdot c_p \cdot (\vartheta_3 - \vartheta_4)$$

Isentropic relation

$$\frac{\vartheta_3}{\vartheta_{4,is}} = \left(\frac{p_3}{p_4} \right)^{\frac{(\kappa-1)}{\kappa}} = \Pi_t^{\frac{(\kappa-1)}{\kappa}}$$

Isentropic efficiency

$$\eta_t = \frac{\vartheta_3 - \vartheta_4}{\vartheta_3 - \vartheta_{4,is}}$$

Turbine exit temperature

$$\vartheta_4 = \vartheta_3 \cdot \left[1 - \eta_t \cdot \left(1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right) \right]$$

Turbine power produced

$$P_t = \dot{m}_t \cdot c_p \cdot \vartheta_3 \cdot \left[1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right] \cdot \eta_t$$

Turbine – Outputs

- **Temperature** of the flow exiting the turbine

$$\vartheta_t = \vartheta_3 \cdot \left[1 - \eta_t \cdot \left(1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right) \right]$$

- **Mass Flow** through the turbine

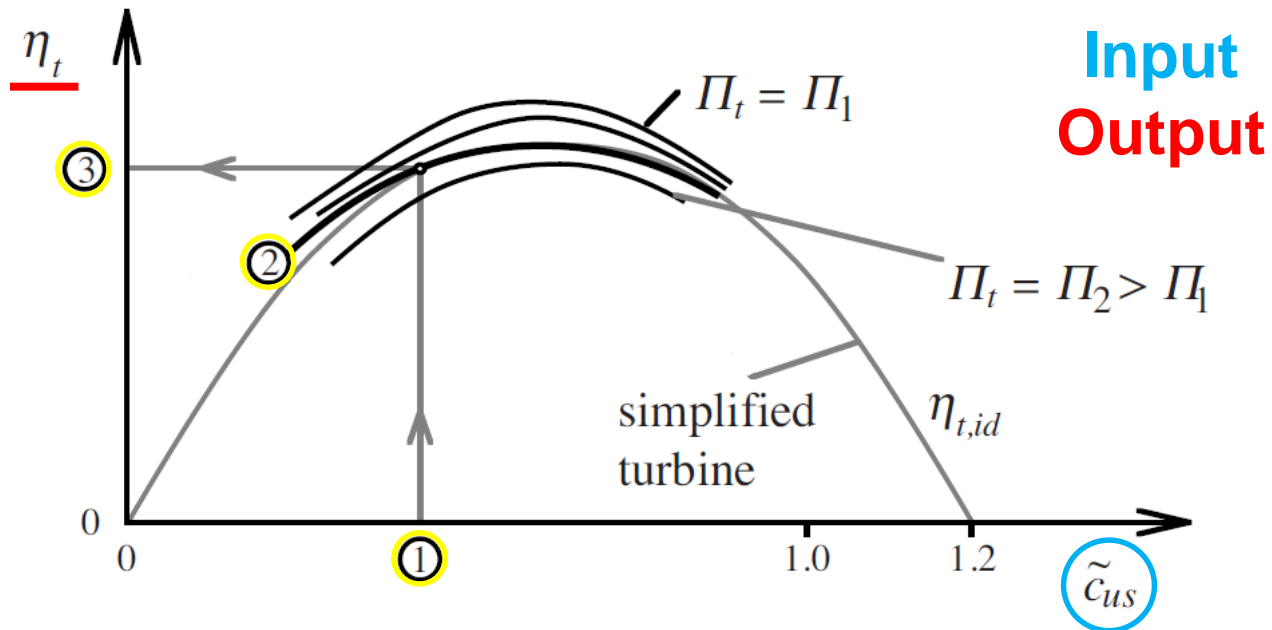
$$\dot{m}_t = \frac{p_3}{p_{ref,0}} \cdot \sqrt{\frac{\vartheta_{ref,0}}{\vartheta_3}} \cdot \dot{\mu}_t$$

$$\Pi_t = \frac{p_3}{p_4} = \frac{p_{bef,t}}{p_{aft,t}}$$

- **Torque** produced by the turbine

$$T_t = \frac{P_t}{\omega_t} = \frac{\dot{m}_t \cdot c_p \cdot \vartheta_3}{\omega_t} \cdot \left[1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right] \cdot \eta_t$$

Turbine – Efficiency Map

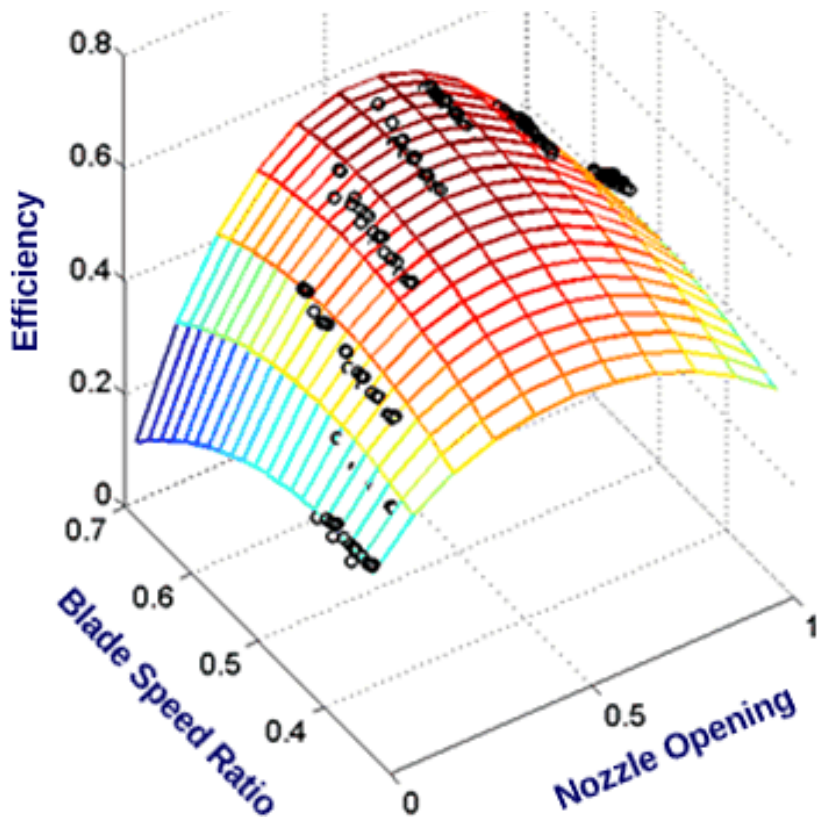


$$c_{us} = \sqrt{2 \cdot c_p \cdot \vartheta_3 \cdot \left[1 - \Pi_t^{(1-\kappa)/\kappa} \right]} \quad \longrightarrow \quad \boxed{\tilde{c}_{us} = \frac{r_t \cdot \omega_t}{c_{us}}}$$

- Since the turbine efficiency mainly depends on the angle of incidence of the inflowing gas, the **turbine blade speed ratio** \tilde{c}_{us} is used as variable.

Turbine – Efficiency Map

Variable Geometry



Source: https://www.dieselnet.com/tech/air_turbo_vgt.php

Turbine – Outputs

- **Temperature** of the flow exiting the turbine

$$\vartheta_t = \vartheta_3 \cdot \left[1 - \eta_t \cdot \left(1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right) \right]$$

- **Mass Flow** through the turbine

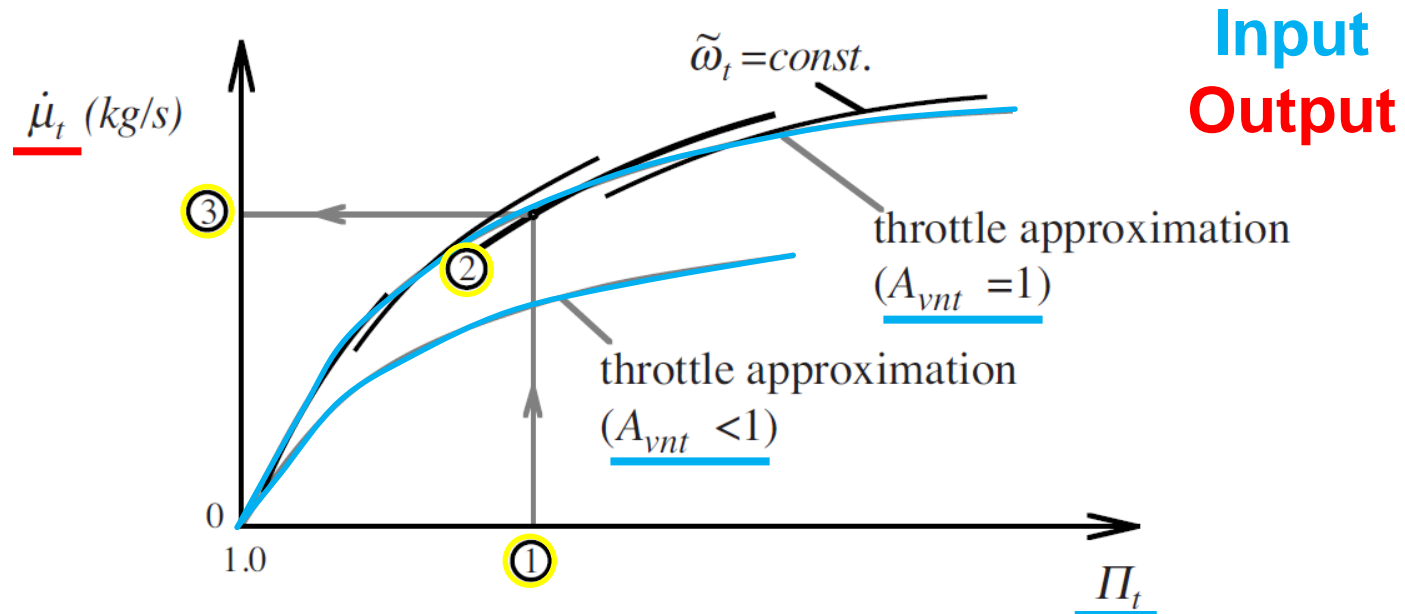
$$\dot{m}_t = \frac{p_3}{p_{ref,0}} \cdot \sqrt{\frac{\vartheta_{ref,0}}{\vartheta_3}} \cdot \dot{\mu}_t$$

$$\Pi_t = \frac{p_3}{p_4} = \frac{p_{bef,t}}{p_{aft,t}}$$

- **Torque** produced by the turbine

$$T_t = \frac{P_t}{\omega_t} = \frac{\dot{m}_t \cdot c_p \cdot \vartheta_3}{\omega_t} \cdot \left[1 - \Pi_t^{\frac{1-\kappa}{\kappa}} \right] \cdot \eta_t$$

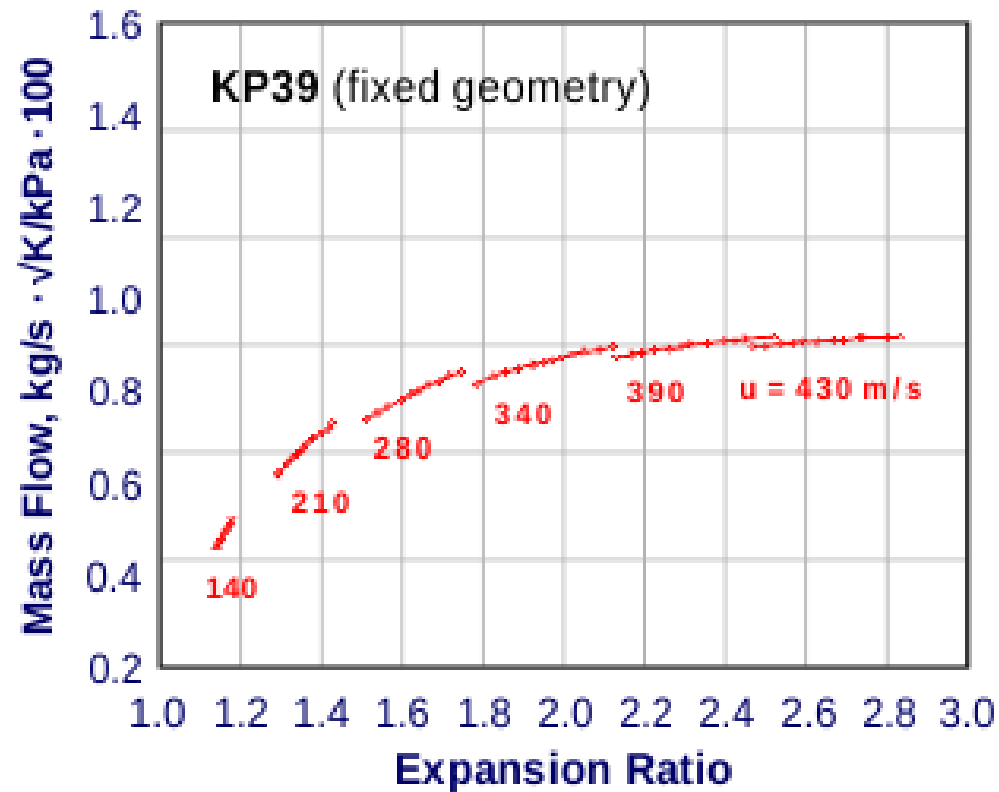
Turbine – Mass Flow Map



- For control purposes, the mass flow behaviour of fluid-dynamic turbines can be modeled quite well as orifice → compressible flow through a valve.
- If the turbine is a Variable Nozzle Turbine (VNT) or Variable Geometry Turbine (VGT), the mass flow and its maximum value depend on the nozzle position (as it is for the compressible flow through a valve).

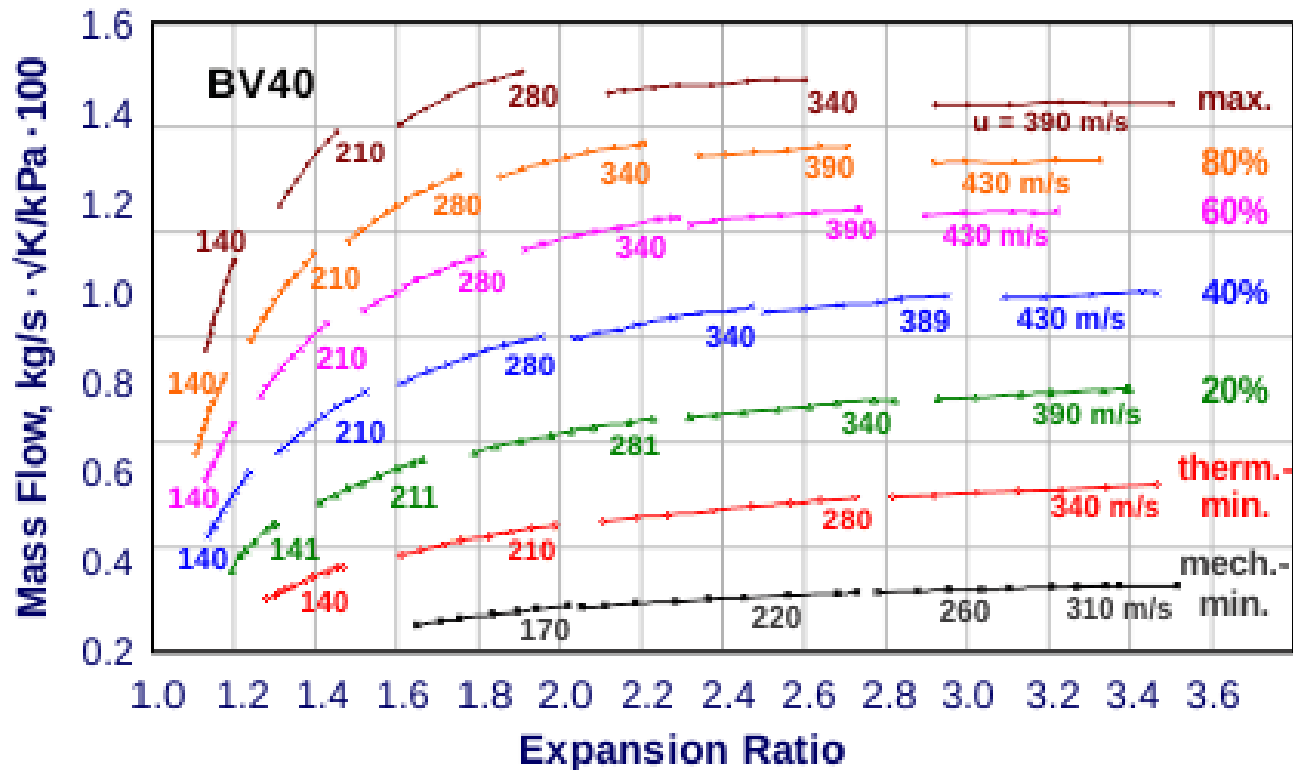
Turbine – Mass Flow Map

Fixed Geometry

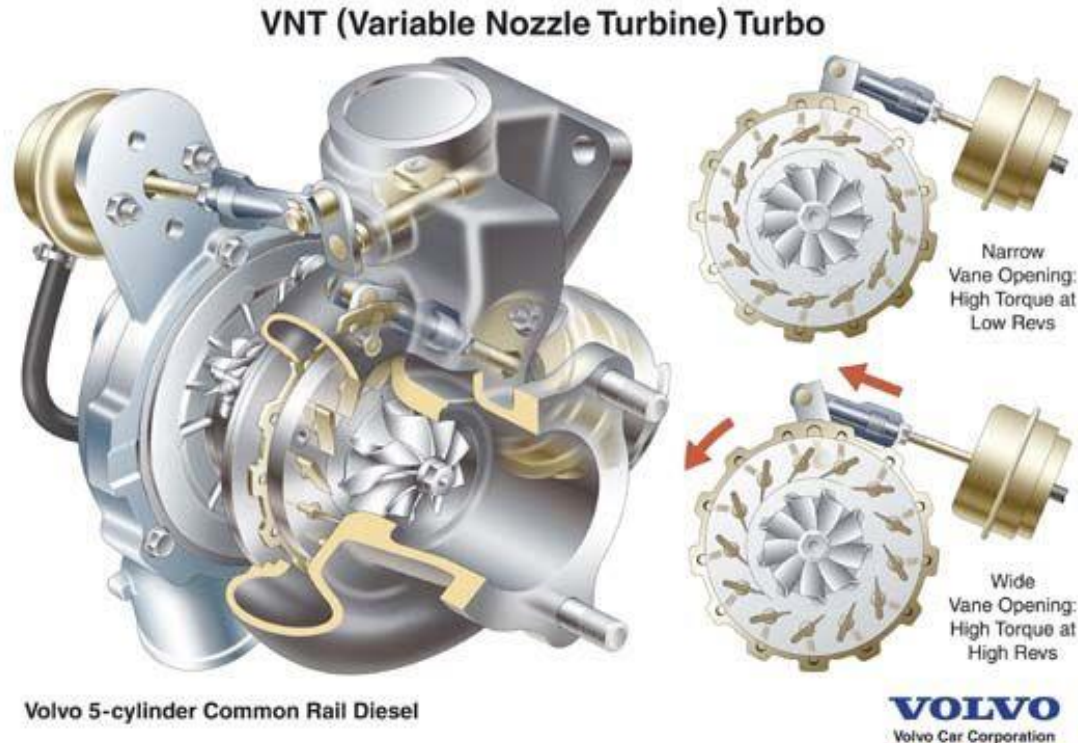


Turbine – Mass Flow Map

Variable Geometry



Turbine – Variable Geometry Turbine (VGT)



At Low Engine Speed

- low mass flow
- low pressure
- low turbine power

Narrow inlet area

- Better incidence
- Increased efficiency
- Increased power

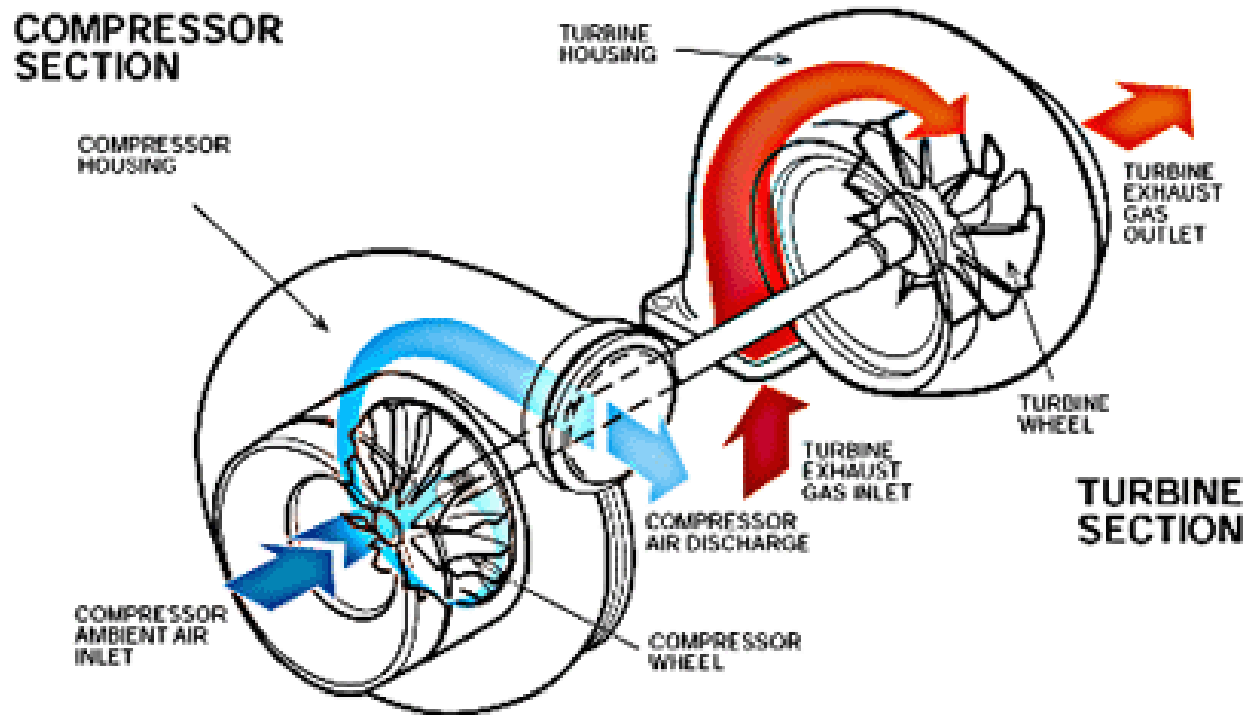
At High Engine Speed

- high mass flow
- high pressure

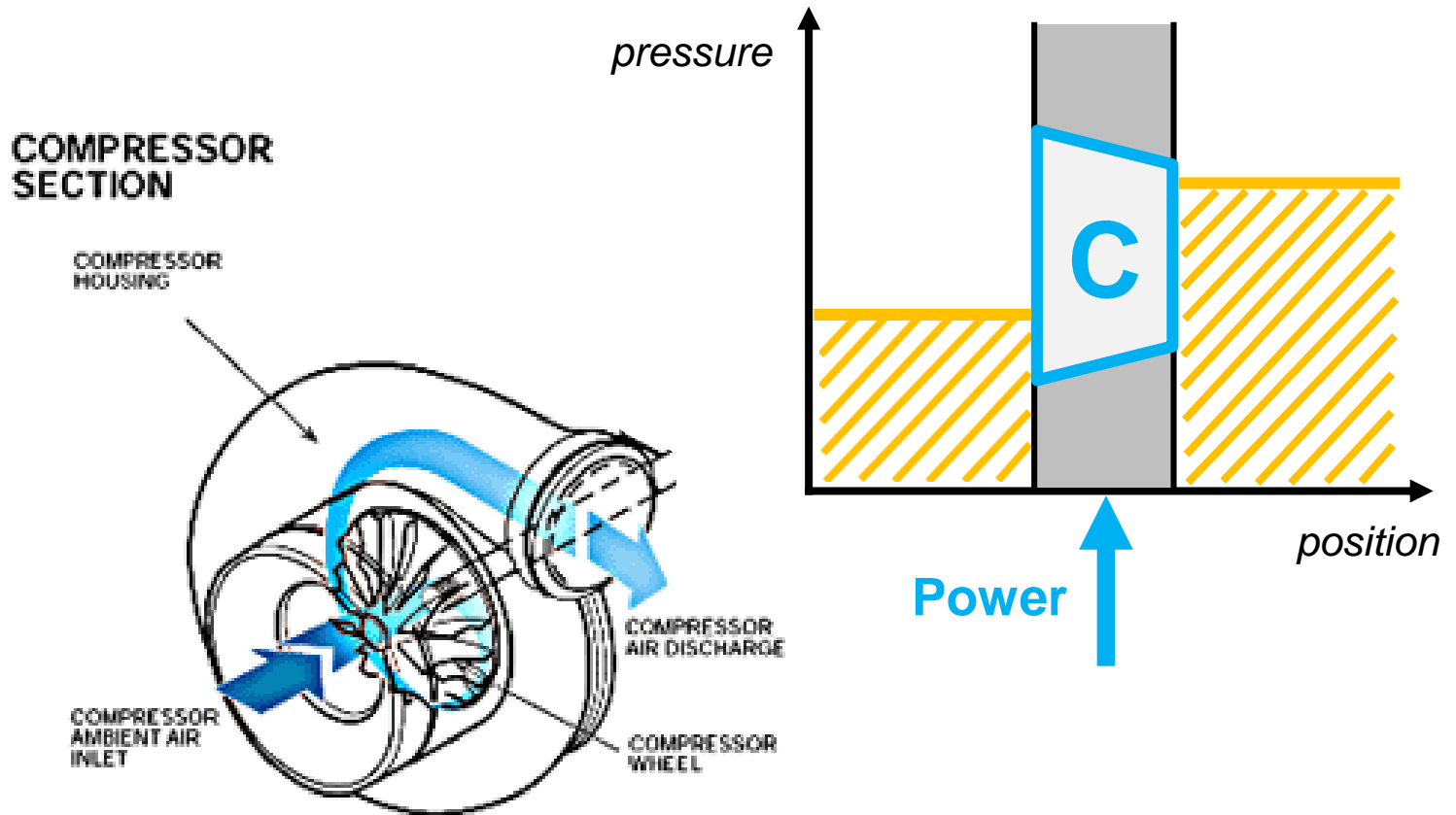
Wide inlet area

- Avoid choke!

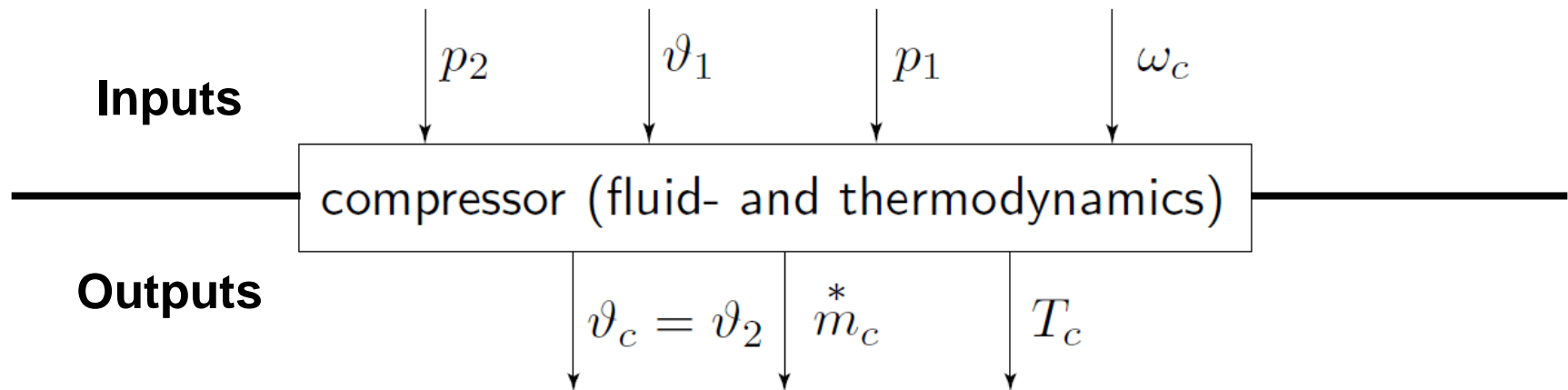
Compressor



Compressor



Compressor – Causality Diagram

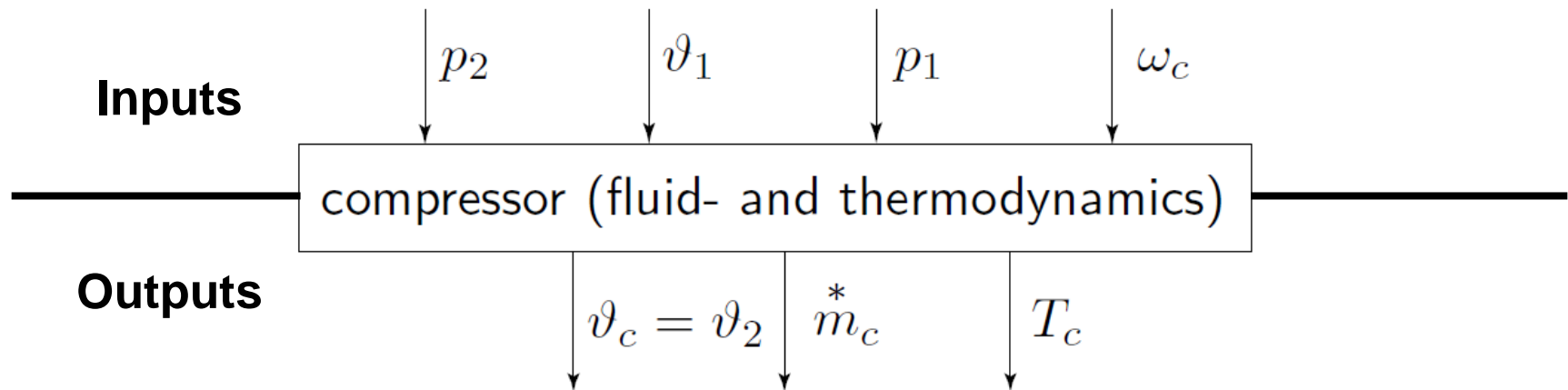


Inputs

- p_1 : Pressure before the compressor [Pa]
- p_2 : Pressure after the compressor [Pa]
- ϑ_1 : Temperature before the compressor [K]
- ω_c : Compressor speed [rad/s]

$$\left. \begin{array}{l} p_1 \\ p_2 \end{array} \right\} \Pi_c = \frac{p_2}{p_1} = \frac{p_{aft,c}}{p_{bef,c}}$$

Compressor – Causality Diagram



Outputs

- ϑ_c : Temperature of the flow exiting the compressor [K]
- \dot{m}_c : Mass flow through the compressor [Kg/s]
- T_c : Torque absorbed by the compressor [Nm]

Compressor – Outputs

- **Temperature** of the flow exiting the compressor

$$\vartheta_c = \vartheta_1 + \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{\vartheta_1}{\eta_c}$$

- **Mass Flow** through the compressor

$$\dot{m}_c = \frac{p_1}{p_{ref,0}} \cdot \sqrt{\frac{\vartheta_{ref,0}}{\vartheta_1}} \cdot \dot{\mu}_c$$

$$\Pi_c = \frac{p_2}{p_1} = \frac{p_{aft,c}}{p_{bef,c}}$$

- **Torque** absorbed by the compressor

$$T_c = \frac{P_c}{\omega_c} = \frac{\dot{m}_c \cdot c_p \cdot \vartheta_1}{\omega_c} \cdot \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{1}{\eta_c}$$

Compressor – Outputs derivation

Open system

$$\frac{dE}{dt} = \dot{H}_{in} - \dot{H}_{out} - \dot{W}_c + \dot{Q}$$

- Compressor does **not store energy** over time $\Rightarrow \frac{dE}{dt} = 0$
- Compressor is assumed to be **adiabatic** (no heat transfer) $\Rightarrow \dot{Q} = 0$

$$P_c = -\dot{W}_c = \dot{H}_{out} - \dot{H}_{in} = \dot{m}_c \cdot c_p \cdot (\vartheta_2 - \vartheta_1)$$

Isentropic relation

$$\frac{\vartheta_{2,is}}{\vartheta_1} = \left(\frac{p_2}{p_1} \right)^{\frac{(\kappa-1)}{\kappa}} = \Pi_c^{\frac{(\kappa-1)}{\kappa}}$$

Isentropic efficiency

$$\eta_c = \frac{\vartheta_{2,is} - \vartheta_1}{\vartheta_2 - \vartheta_1}$$

Compressor exit temperature

$$\vartheta_2 = \vartheta_1 + \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{\vartheta_1}{\eta_c}$$

Compressor power absorbed

$$P_c = \dot{m}_c \cdot c_p \cdot \vartheta_1 \cdot \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{1}{\eta_c}$$

Compressor – Outputs

- **Temperature** of the flow exiting the compressor

$$\vartheta_c = \vartheta_1 + \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{\vartheta_1}{\eta_c}$$

- **Mass Flow** through the compressor

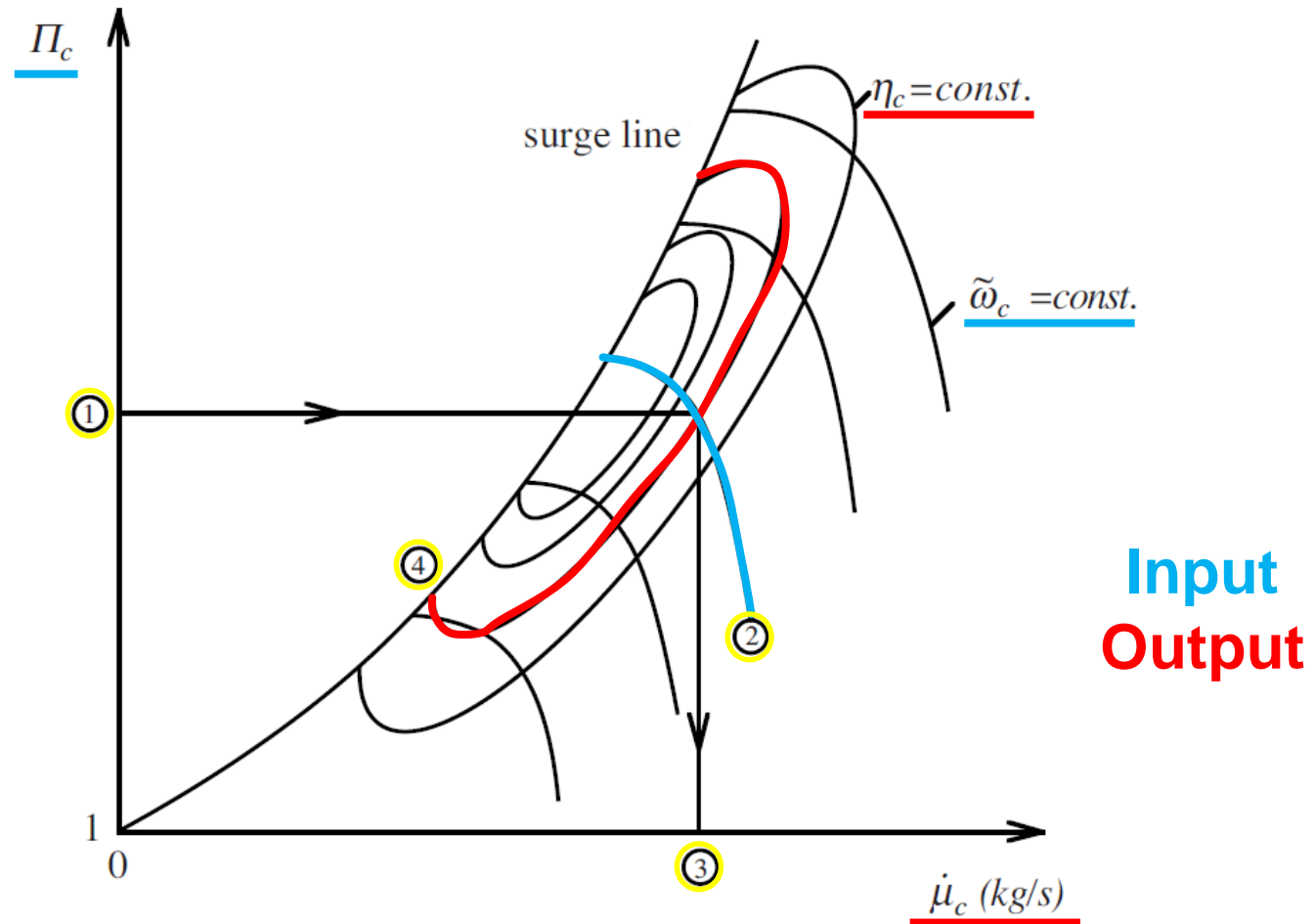
$$\dot{m}_c = \frac{p_1}{p_{ref,0}} \cdot \sqrt{\frac{\vartheta_{ref,0}}{\vartheta_1}} \cdot \dot{\mu}_c$$

$$\Pi_c = \frac{p_2}{p_1} = \frac{p_{aft,c}}{p_{bef,c}}$$

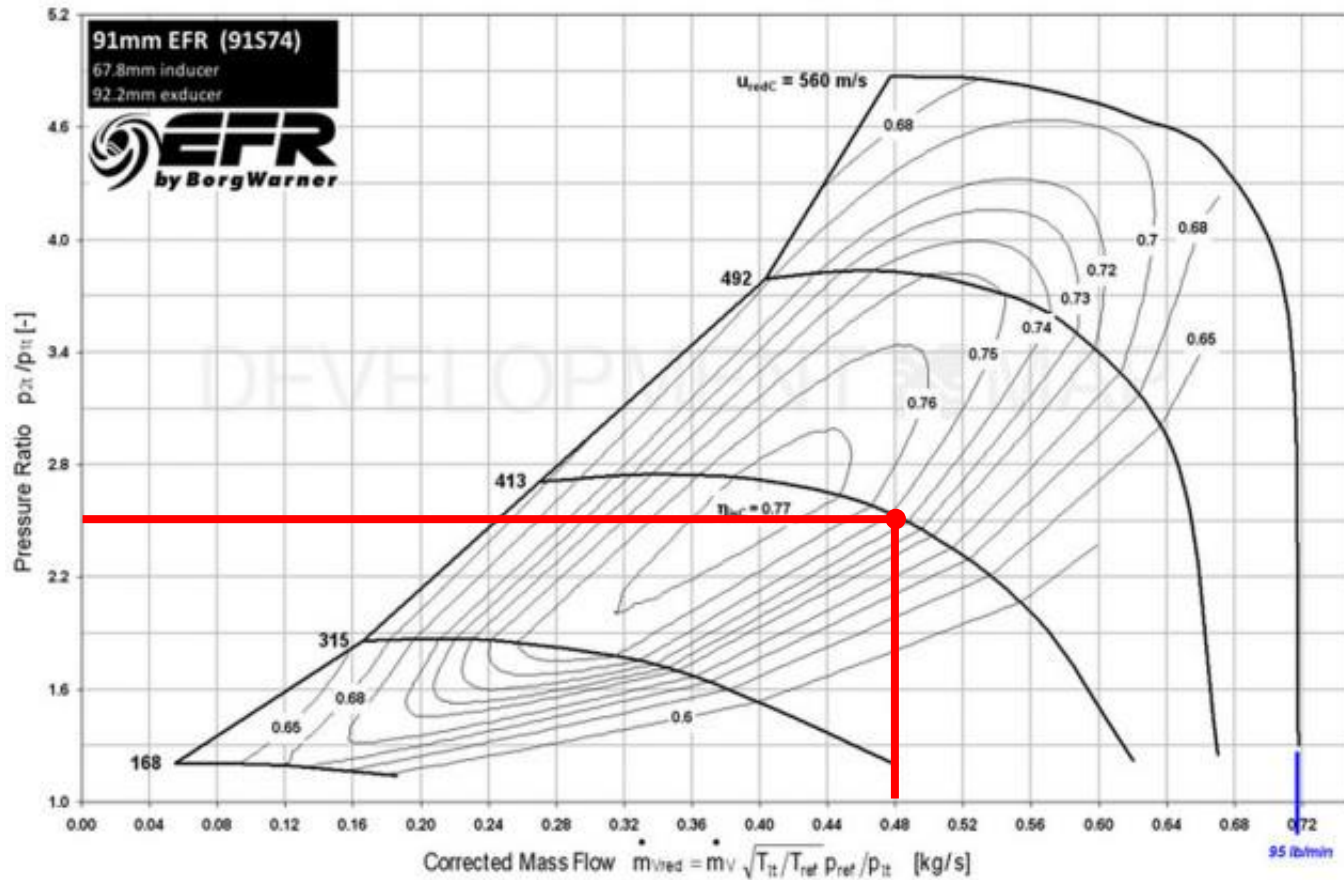
- **Torque** absorbed by the compressor

$$T_c = \frac{P_c}{\omega_c} = \frac{\dot{m}_c \cdot c_p \cdot \vartheta_1}{\omega_c} \cdot \left[\Pi_c^{\frac{\kappa-1}{\kappa}} - 1 \right] \cdot \frac{1}{\eta_c}$$

Compressor – Mass Flow & Efficiency Map

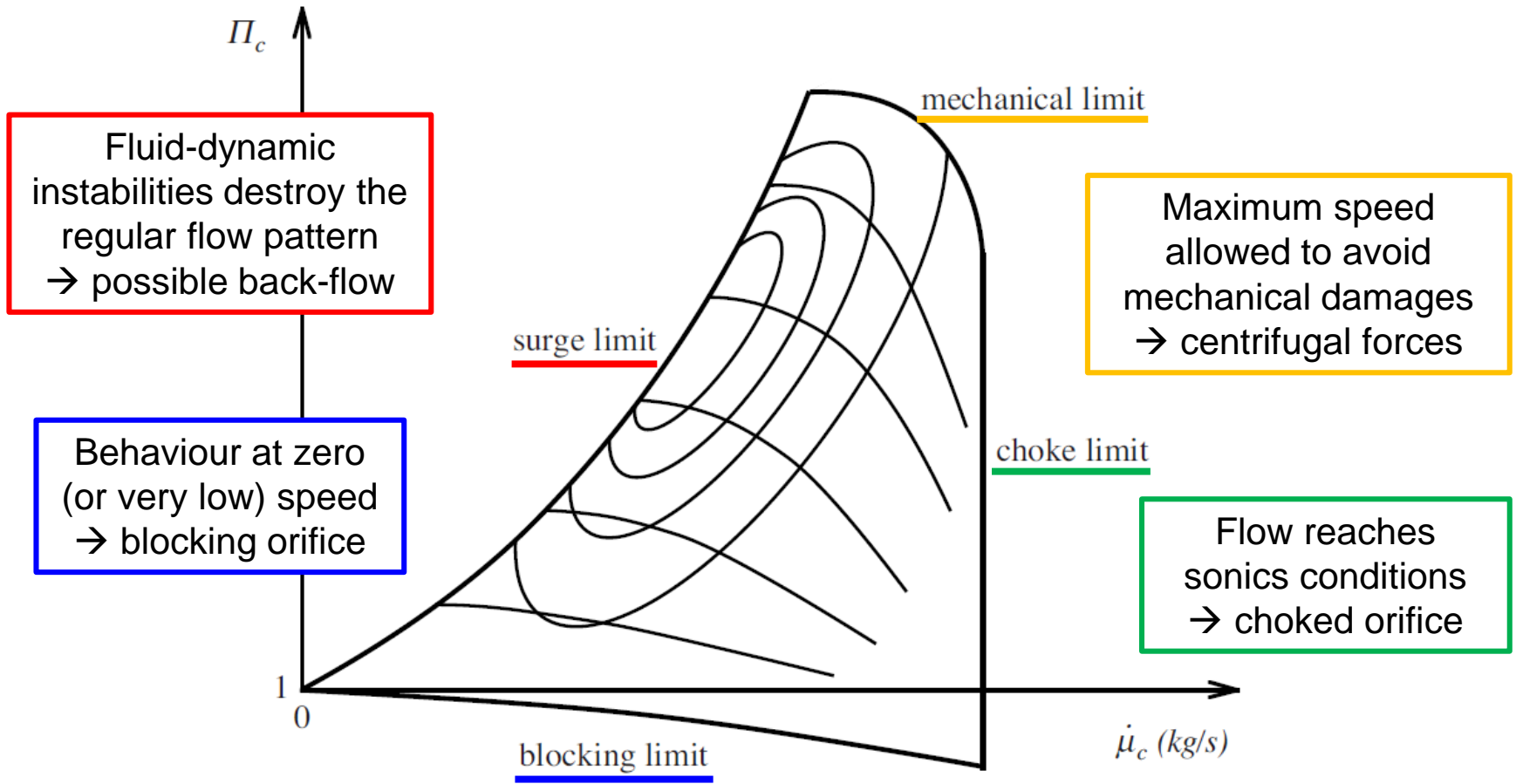


Compressor – Mass Flow & Efficiency Map

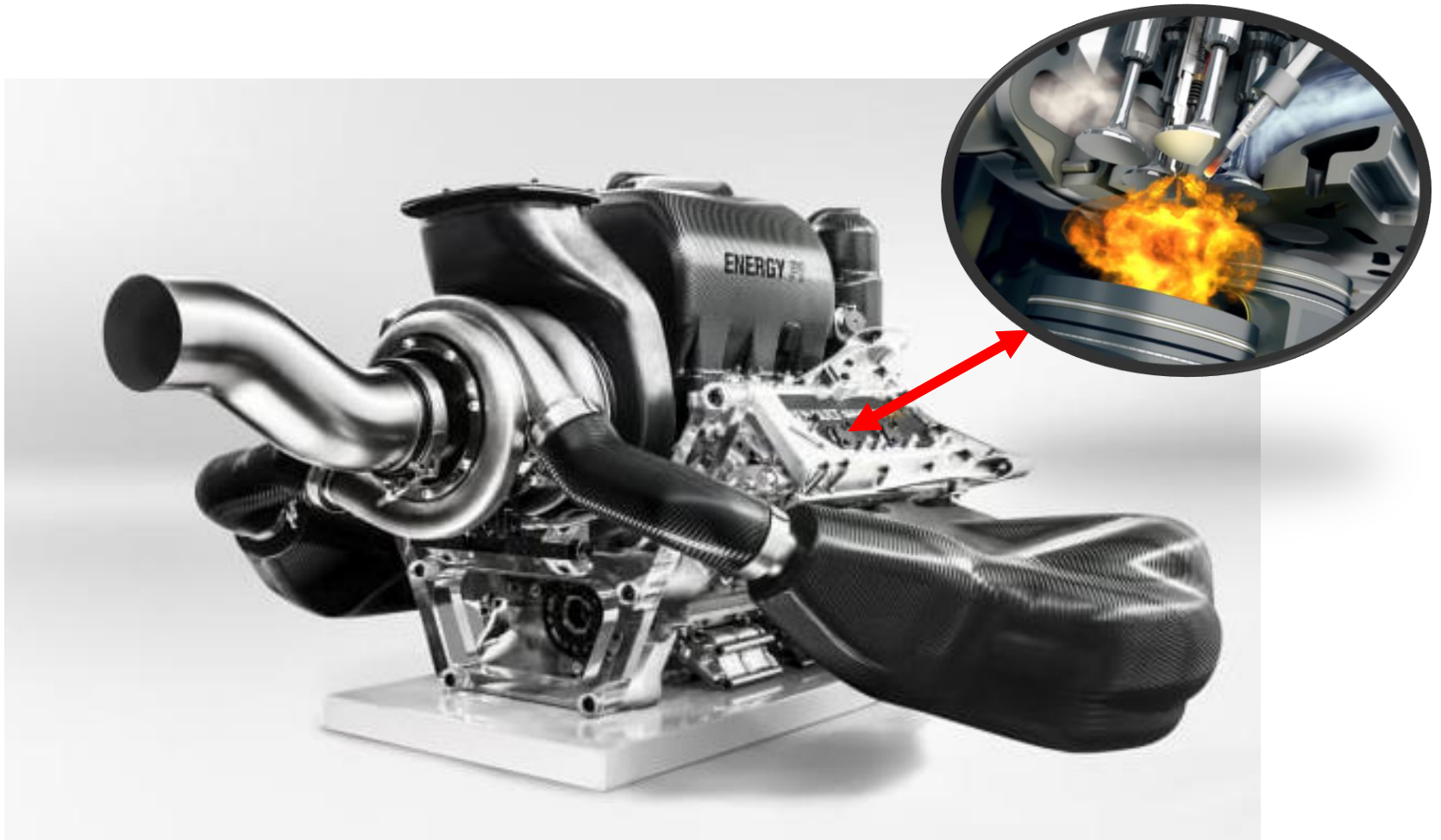


Source: <http://www.engine-labs.com/engine-tech/power-adders/understanding-compressor-maps-sizing-a-turbocharger/>

Compressor – Operational Limits



Formula 1 – Turbocharged Engine



Source: <https://sport.sky.it/formula1/2017/03/21/formula-1--il-dizionario--power-unit-ed-elettronica.html>

Internal Combustion Engine

Engine Power can be approximated as following:

$$P_{engine} = P_{comb,fuel} + P_{fric} + P_{pump}$$

Assume constant engine speed ω_e

- **Engine Power** coming from the **fuel combustion**:

$$P_{comb,fuel} = e_{comb} \cdot P_f = e_{comb} \cdot H_l \cdot \dot{m}_{fuel} \approx \underline{k_1 \cdot \dot{m}_{fuel}}$$

- **Engine Power** coming from the pistons **mechanical friction**:

$$P_{fric} \approx \underline{k_2}$$

- **Engine Power** coming from the **gas exchange**:

$$P_{pump} = (p_{intake} - p_{exhaust}) \cdot V_d \cdot \frac{\omega_e}{4\pi} \approx \underline{k_3 \cdot (p_{intake} - p_{exhaust})}$$

Internal Combustion Engine

- **Engine Power**, neglecting the friction and assuming $p_{intake} = p_{exhaust}$:

$$P_{engine} \approx k_1 \cdot \dot{m}_{fuel} + k_3 \cdot (p_{intake} - p_{exhaust}) \approx k_1 \cdot \dot{m}_{fuel}$$

- **Air to Fuel Ratio** is defined as following:

$$\lambda_{AF} = \frac{\dot{m}_{air}}{\dot{m}_{fuel}} \cdot \frac{1}{\sigma_0} \quad \xrightarrow{\lambda_{AF} = 1} \quad \dot{m}_{fuel} = \frac{\dot{m}_{air}}{\sigma_0}$$

- **Engine Air Mass Flow** is approximated as following:

$$\dot{m}_{air} = \frac{p_{intake}}{R_{air} \cdot \vartheta_{intake}} \cdot \frac{\omega_e}{4\pi} \cdot V_d \cdot \lambda_{vol} \approx k_4 \cdot p_{intake}$$

$$P_{engine} \propto \dot{m}_{fuel} \propto \dot{m}_{air} \propto p_{intake}$$

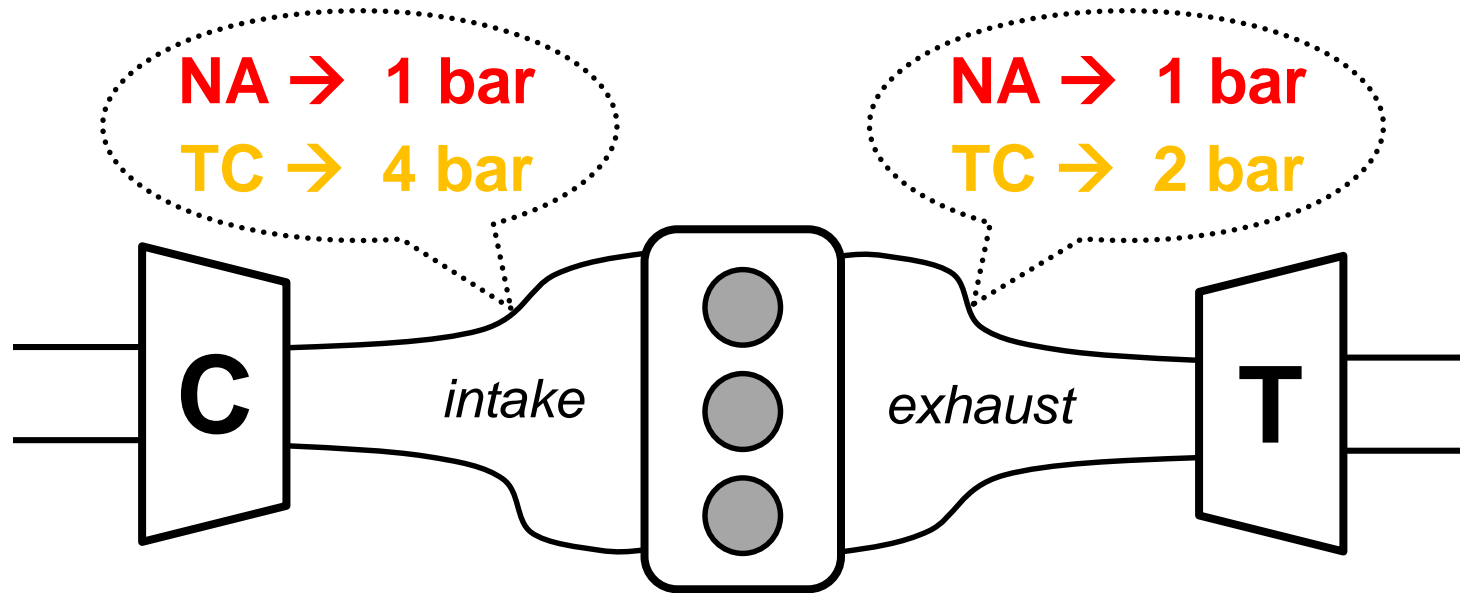
NA → 1 bar → 100 kW

TC → 4 bar → 400 kW

Turbocharged Engine

- **Engine Power**, neglecting the friction and for a specific \dot{m}_{fuel} :

$$P_{engine} \approx k_1 \cdot \dot{m}_{fuel} + k_3 \cdot (p_{intake} - p_{exhaust})$$



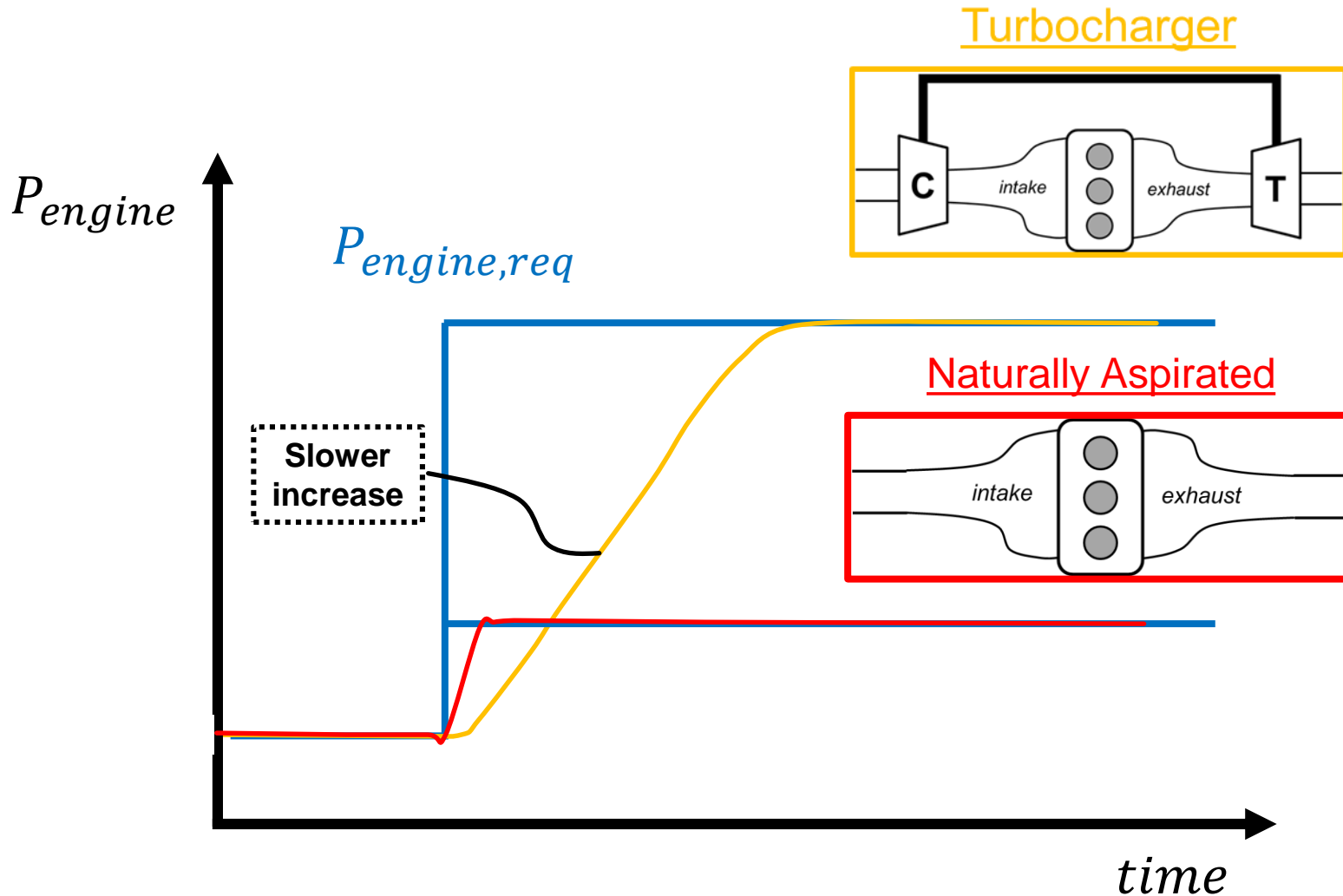
$$\omega_e = 10'000 \text{ rpm}$$

$$V_d = 1.6 \text{ L}$$

$$P_{pump,NA} \approx 0 \text{ kW}$$

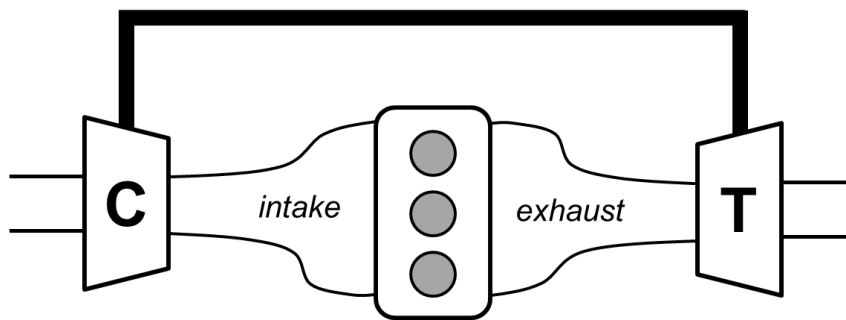
$$P_{pump,TC} \approx 26 \text{ kW}$$

Engine Response

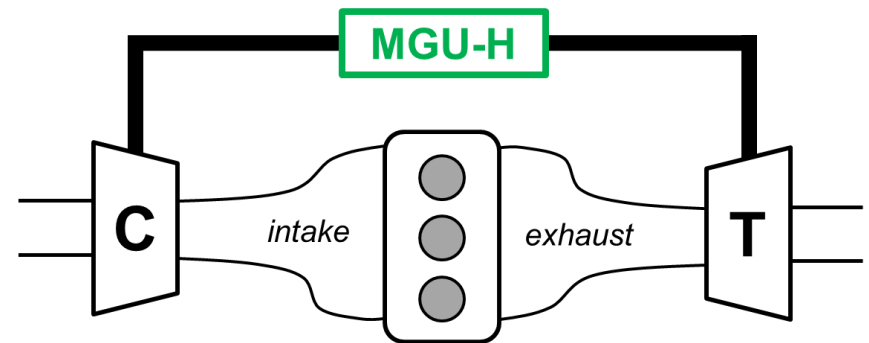


Formula 1 – Engine Response

How and how fast is the **engine power response** of a **conventional turbocharger** compared to an **electrified turbocharger** (e.g. F1) ?



Turbocharger

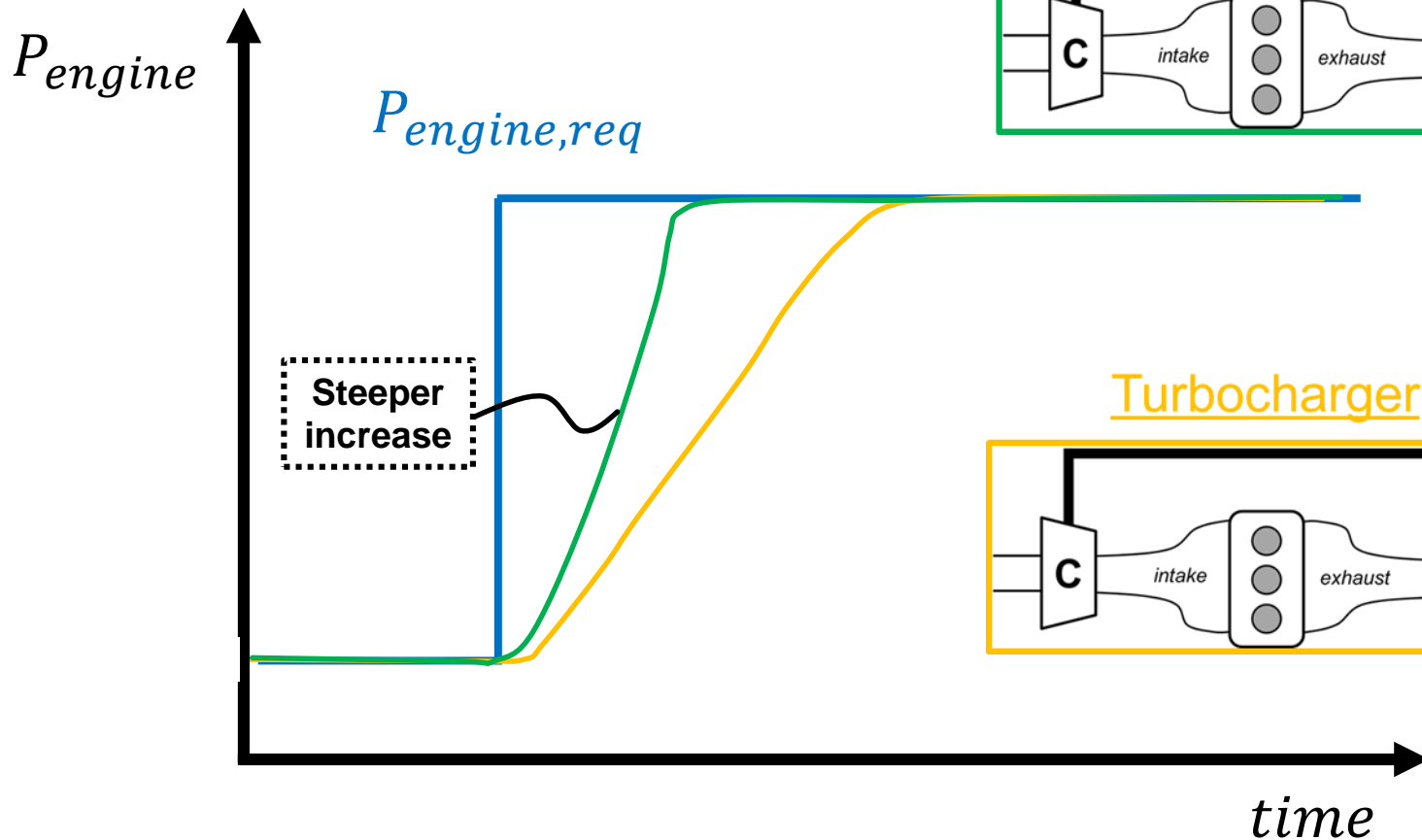


Electrified Turbocharger

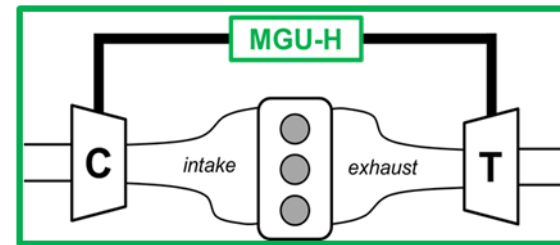
- 1) Press throttle pedal
- 2) More fuel injected
- 3) Exhaust temperature increases
- 4) More power extracted by the turbine
- 5) Turbocharger speed increases
- 6) Compressor mass flow increases
- 7) More air → more fuel can be injected
- 8) More Engine power

- 1) Press throttle pedal
- 2) More fuel injected & MGU-H positive
- 3) Turbocharger speed increases faster (→ MGU-H & exhaust temperature)
- 4) Compressor mass flow increases
- 5) More air → more fuel can be injected
- 6) More Engine power

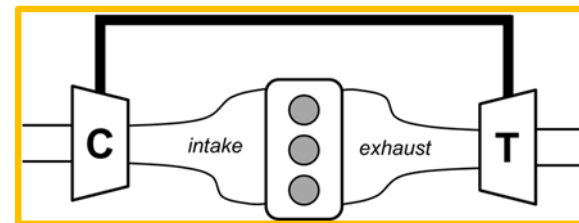
Formula 1 – Engine Response



Electrified Turbocharger



Turbocharger



IDSC Open Lab 2017

ETH zürich

Open Lab 2017

Date:

Thursday, 9. November, 2017

Time:

18:00 - 20:00

Location:

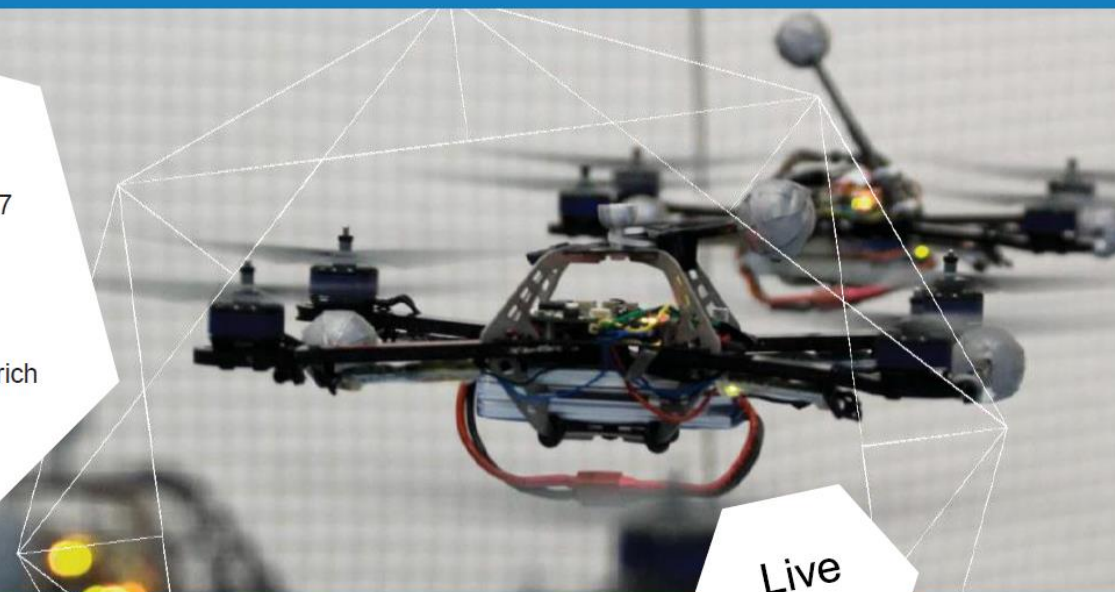
ML Building
Sonneggstrasse 3, 8092 Zurich

Opening:

ML E 12

Demos:

Various locations



Live
Demos

Open Lab 2017

Institute for Dynamic Systems and Control

Prof. R. D'Andrea, Prof. E. Frazzoli, Prof. Ch. Onder, Prof. M. Zeilinger



IDSC Open Lab 2017



ML K37.1

Formula 1 Power Unit

Efficient control algorithms are designed for the hybrid electric propulsion system of the Formula 1 car, in order to achieve the fastest possible lap-time. (Presentations in English or German)

Mauro Salazar, maurosalar@idsc.mavt.ethz.ch |
Camillo Balerna, balernac@idsc.mavt.ethz.ch

<http://www.idsc.ethz.ch/research-guzzella-ponder/research-projects/Formula1.html>